

An Improved Third Order Vertical Advection Scheme for the Runge-Kutta Dynamical Core

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Motivation:

in a convection-permitting model (like COSMO-DE) the vertical advection plays a much bigger role than in a convection-parameterising model

→ try to achieve higher accuracy in the vertical advection of dynamic variables (u, v, w, T', p'), too

COSMO-model up to now: vertically implicit centered diff. 2nd order

WRF: vertically explicit upwind scheme (3rd order)

- **advantages:**

- Fits best to the explicit horizontal advection and the Runge-Kutta-scheme
- Relatively easy to implement

- **disadvantages:**

- Limitation of Courant number: $C_x + C_y + C_z < 1.4$ (*Baldauf, 2008, JCP*) →
 - WRF uses smaller time steps (~15 sec for $dx=3\text{km}$)
 - WRF uses a vertical ‘velocity brake’

→ **Keep the vertically implicit scheme, but try a higher order of approximation**

(COSMO priority project 'Runge-Kutta', Task 8)

Several implicit advection schemes (2-timelevels)

$$\frac{\phi^{n+1} - \phi^n}{\Delta t} = \beta A_z(\phi^{n+1}) + (1 - \beta) A_z(\phi^n)$$

To achieve higher order in time, too, we will use $\beta=1/2$ ('pure' Crank-Nicholson)

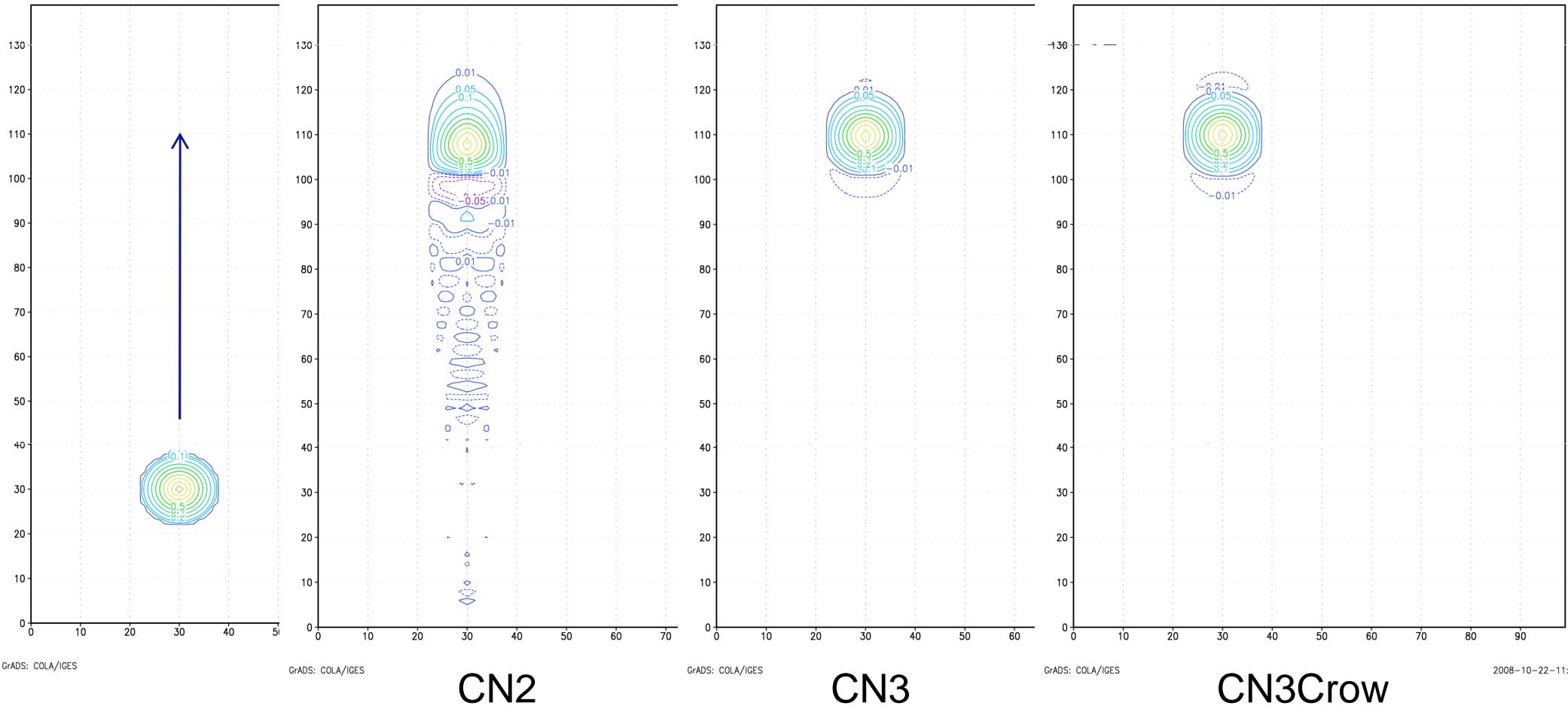
A_z denotes a spatial discretisation of the vertical advection operator:

- Centered differences 2nd order (spatially and temporally) ('CN2') **current**
- Upwind 3rd order (spatially) ('CN3') **new**
- Upwind 3rd order (spatially and temporally) ('CN3Crow') **new**
its derivation is quite analogous to the explicit Crowley-schemes
(Tremback et al., 1987, MWR)

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Pure advection test:

Only implicit scheme (i.e. $u=0$), $w=2$, $dt=0.25 \rightarrow C_z=0.5$



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GrADS: COLA/IGES

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CN2

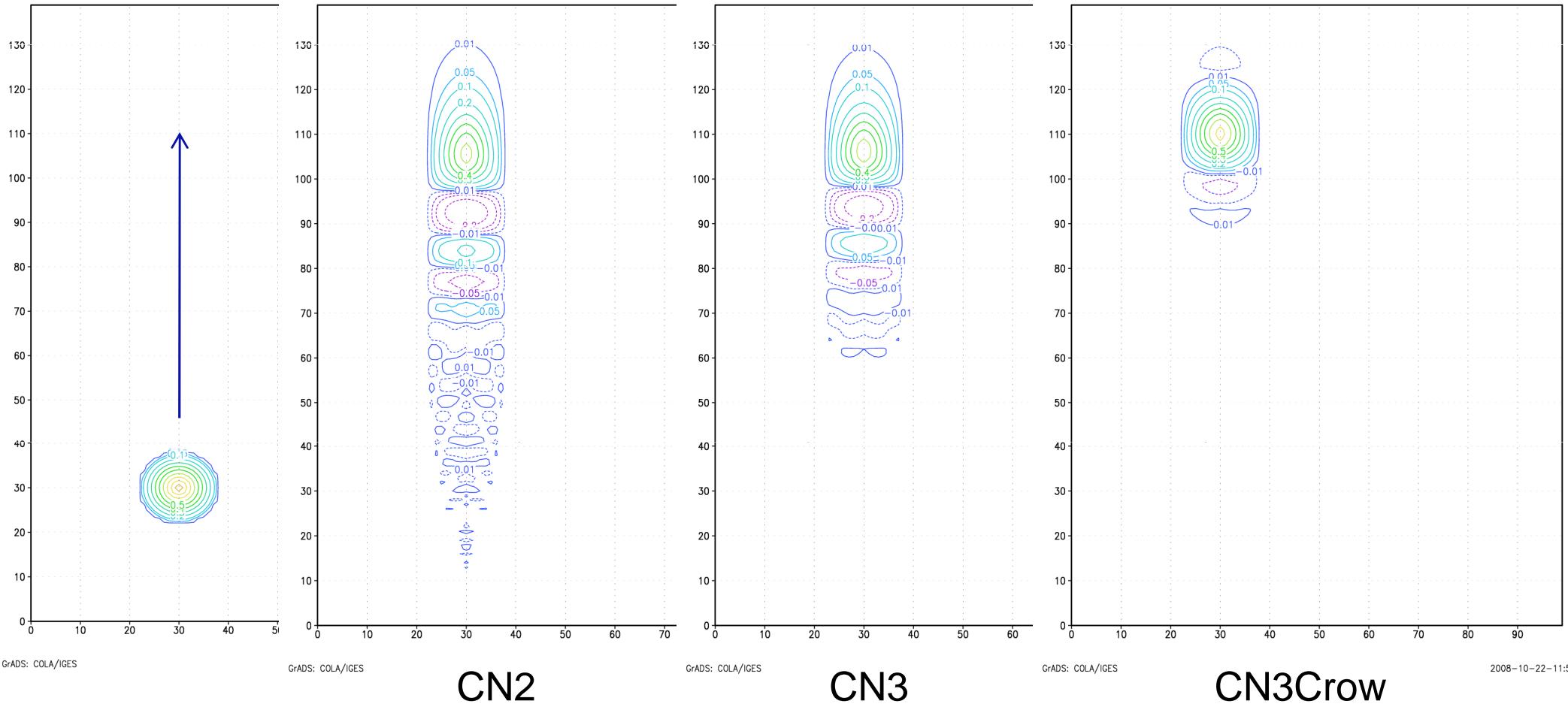
CN3

CN3Crow

Test 20081010_ay

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Pure advection test:
Only implicit scheme (i.e. $u=0$), $w=2$, $dt=1.5 \rightarrow C_z=3$



The current 3-stage RK-scheme in the COSMO-model

Wicker, Skamarock (2002) MWR



solve the implicit scheme: $\frac{\tilde{\phi} - \phi^n}{\frac{\Delta t}{3}} = \beta A_z(\tilde{\phi}) + (1 - \beta) A_z(\phi^n) + A_x(\phi^n) + P(\phi^n)$ (1)

... and define its tendency: $L(\phi^n) := \frac{\tilde{\phi} - \phi^n}{\frac{\Delta t}{3}}$ (2)

1. RK-substep: $\phi^* = \phi^n + \frac{\Delta t}{3} L(\phi^n)$ (3)

fast waves with tendency $\frac{\phi^* - \phi^n}{\Delta t/3}$, starting at $\phi^n \Rightarrow \phi^*$ (4)

solve: $\frac{\tilde{\phi} - [\alpha\phi^n + (1 - \alpha)\phi^*]}{\frac{\Delta t}{2}} = \beta A_z(\tilde{\phi}) + (1 - \beta) A_z(\phi^*) + A_x(\phi^*) + P(\phi^n)$ (5)

... and define its tendency: $L(\phi^*) := \text{lhs. of the above expression}^1$ (6)

2. RK-substep: $\phi^{**} = \phi^n + \frac{\Delta t}{2} L(\phi^*)$ (7)

fast waves with tendency $\frac{\phi^{**} - \phi^n}{\Delta t/2}$, starting at $\phi^n \Rightarrow \phi^{**}$ (8)

solve: $\frac{\tilde{\phi} - [\alpha\phi^n + (1 - \alpha)\phi^{**}]}{\Delta t} = \beta A_z(\tilde{\phi}) + (1 - \beta) A_z(\phi^{**}) + A_x(\phi^{**}) + P(\phi^n)$ (9)

... and define its tendency: $L(\phi^{**}) := \text{lhs. of the above expression}$ (10)

3. RK-substep: $\phi^{n+1} = \phi^n + \Delta t L(\phi^{**})$ (11)

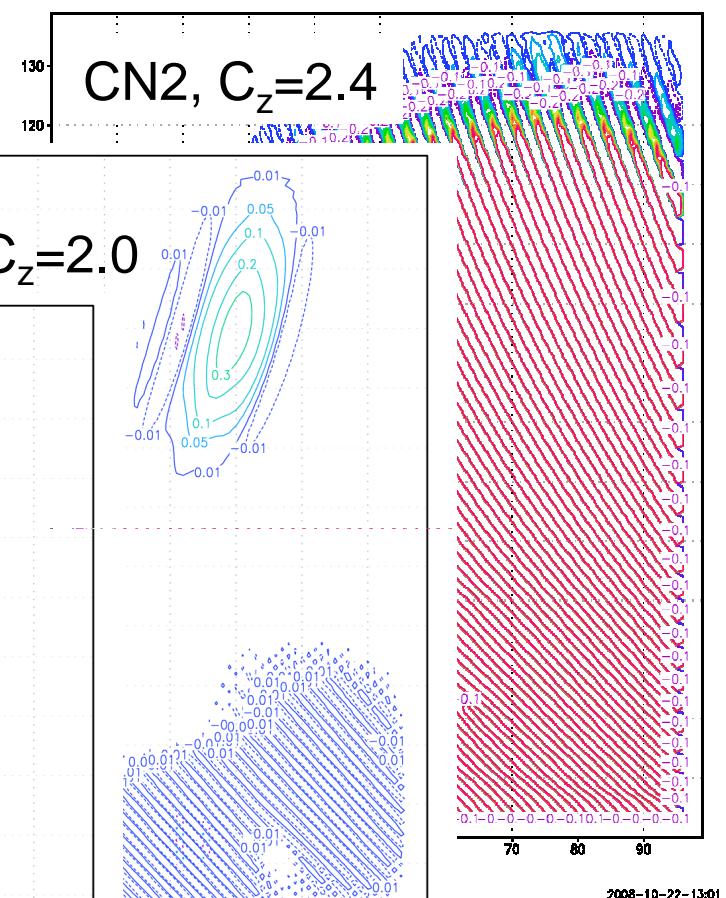
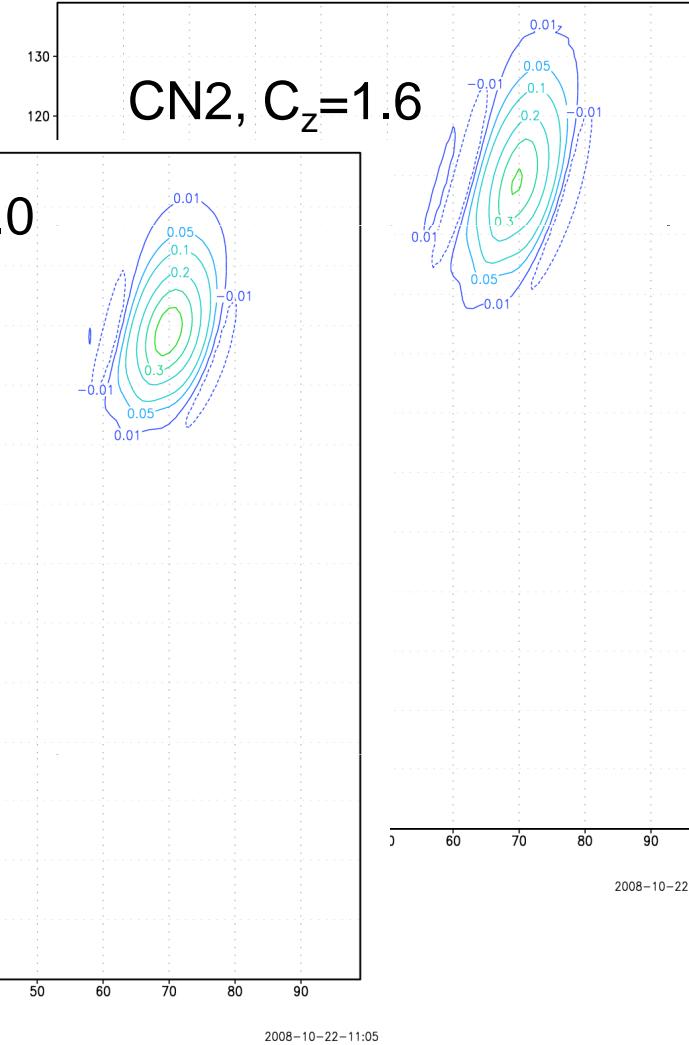
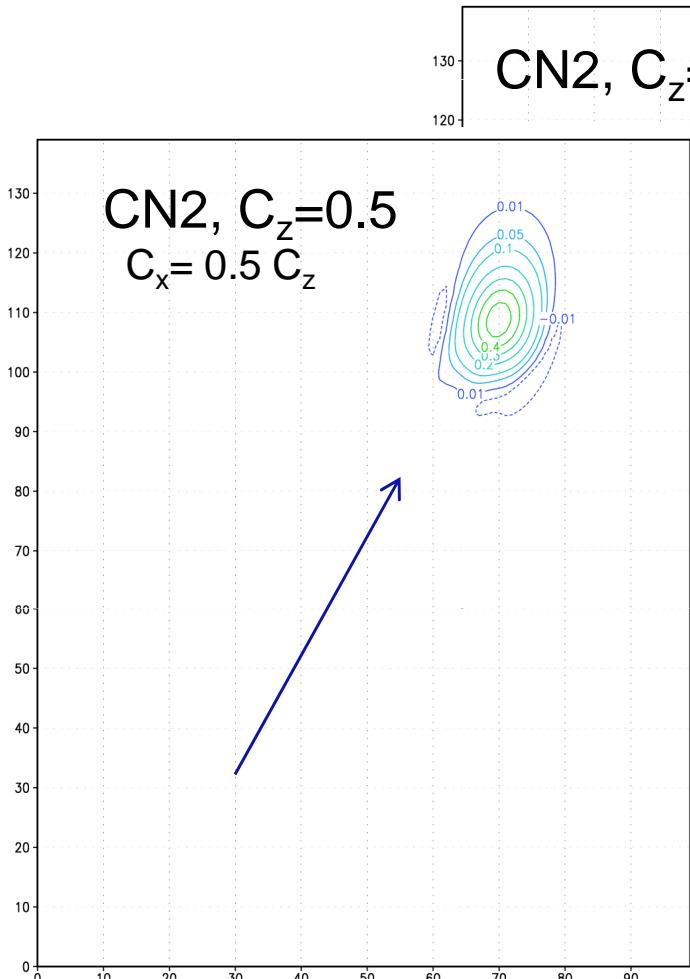
fast waves with tendency $\frac{\phi^{n+1} - \phi^n}{\Delta t}$, starting at $\phi^n \Rightarrow \phi^{n+1}$ (12)

In the following: $A_x = \text{upwind 5}^{\text{th}} \text{ order}$



The current 3-stage RK-scheme in the COSMO-model

Only horizontal + vertical adv.



Test 20081022_a

Conclusions:

- The current scheme shows a certain damping.
This seems to be typically for implicit schemes used inside of a Runge-Kutta-scheme (for the ‘slow’ part) (*Baldauf (2009), submitted to JCP*)
 - The vertical advection is not unconditionally stable,
despite the fact, that an implicit scheme is used
(but up to now this was not a problem in all COSMO-DE or –EU runs)
-

Remark: for $\alpha=0$ (i.e. without an overdamping):

- Bigger dispersion error
- Instability sets in much earlier (at $dt=0.8 \rightarrow C_z=1.6$)

New proposal: complete operator splitting

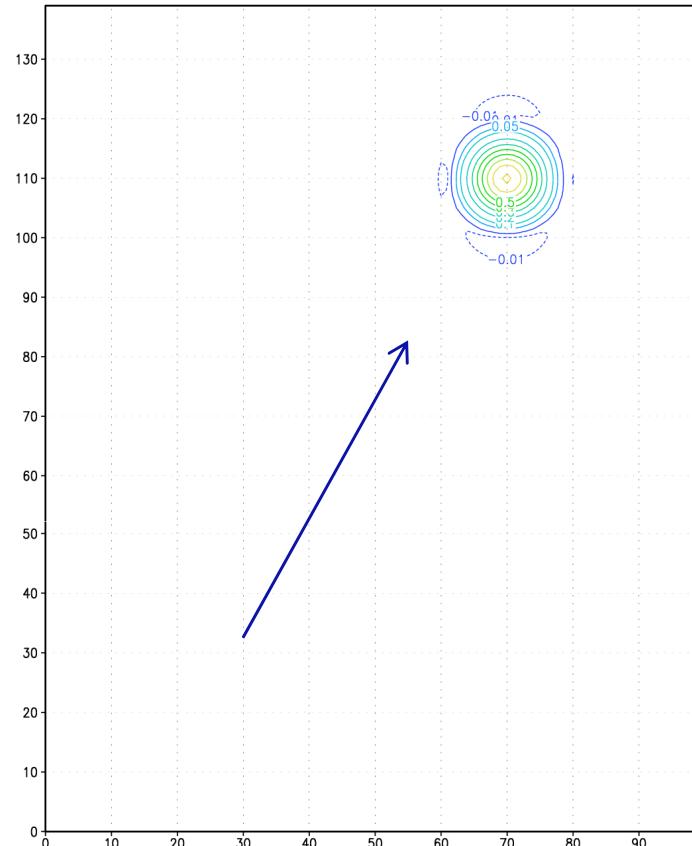
$$\begin{aligned}\frac{\tilde{\phi} - \phi^n}{\Delta t} &= R_x(\phi^n) & R_x = \text{complete RK3-scheme, but without } A_z \\ \frac{\phi^{n+1} - \tilde{\phi}}{\Delta t} &= \beta A_z(\phi^{n+1}) + (1 - \beta) A_z(\tilde{\phi})\end{aligned}$$

advantages:

- no implicit scheme occurs inside of the RK
- if the numerical operators commute, then the stability properties of the single operators are passed on to the whole scheme
(LeVeque and Oliger, 1983)
- 'overdamping' is not needed ($\rightarrow \alpha=0$ is possible)
- 'expensive' vertical advection is called only once / timestep

Complete operator splitting, CN3Crow

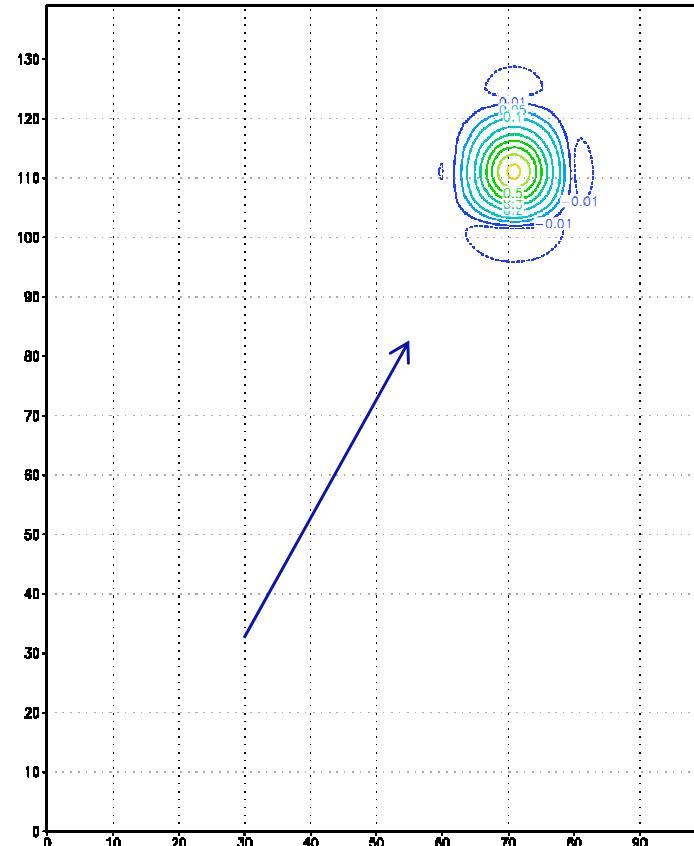
$dt=0.25 \rightarrow C_z=0.5$



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$dt=1.2 \rightarrow C_z=2.4$



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GrADS: COLA/IGES

Test 20081010_a

Question: does the 'complete operator splitting' work together with fast (sound-, gravity-) waves?
(splitting-error, stability, ...)

Linearised shallow water equations

$$\frac{\partial u}{\partial t} + U_0 \frac{\partial u}{\partial x} + V_0 \frac{\partial u}{\partial y} = -g \frac{\partial h}{\partial x} + M_x$$

$$\frac{\partial v}{\partial t} + U_0 \frac{\partial v}{\partial x} + V_0 \frac{\partial v}{\partial y} = -g \frac{\partial h}{\partial y} + M_y$$

$$\frac{\partial h}{\partial t} + U_0 \frac{\partial h}{\partial x} + V_0 \frac{\partial h}{\partial y} = -H_0 D$$

$$\text{with } D = \frac{\partial u}{\partial x} + \frac{\partial v}{\partial y}$$

Divergence damping:

$$M_x = \alpha_{Div} \frac{\partial D}{\partial x}$$

$$M_y = \alpha_{Div} \frac{\partial D}{\partial y}$$

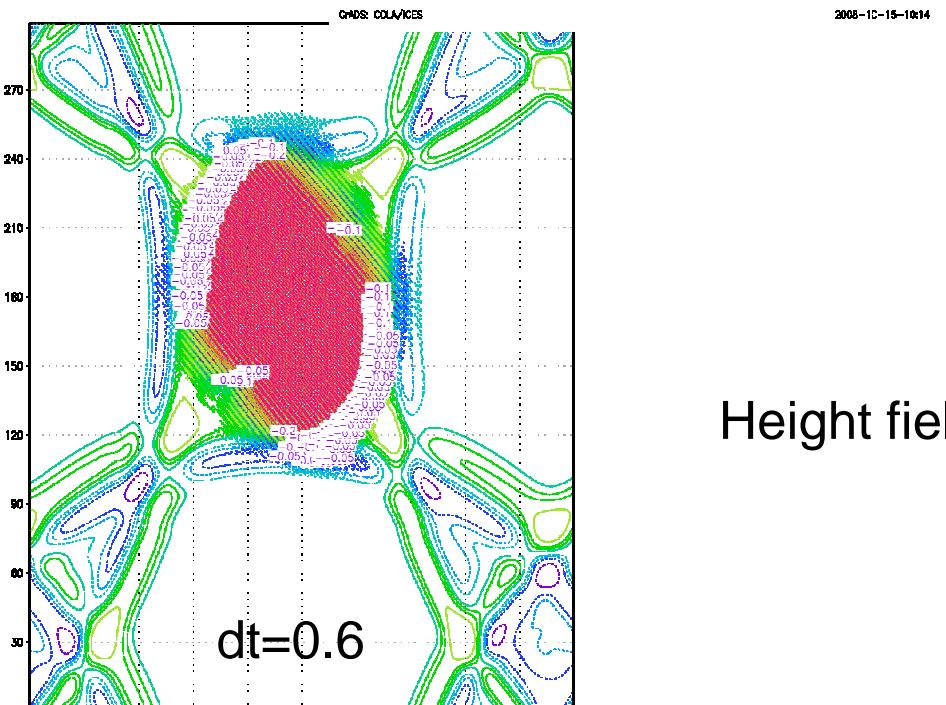
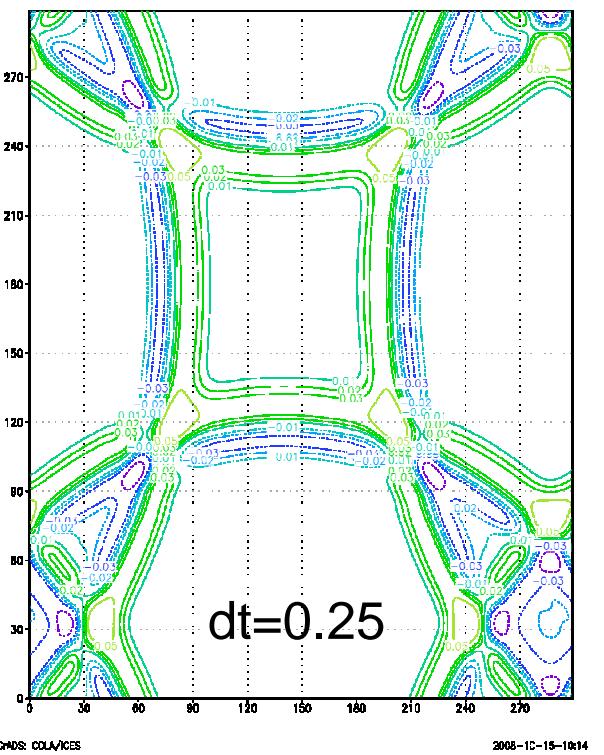
Advective transport with velocity (U_0, V_0)

fast wave expansion with velocity $c_{wav} = \sqrt{gH_0}$

Here: apply the new implicit advection to the y-direction

For reference:

upwind5
in y-direction



Height field

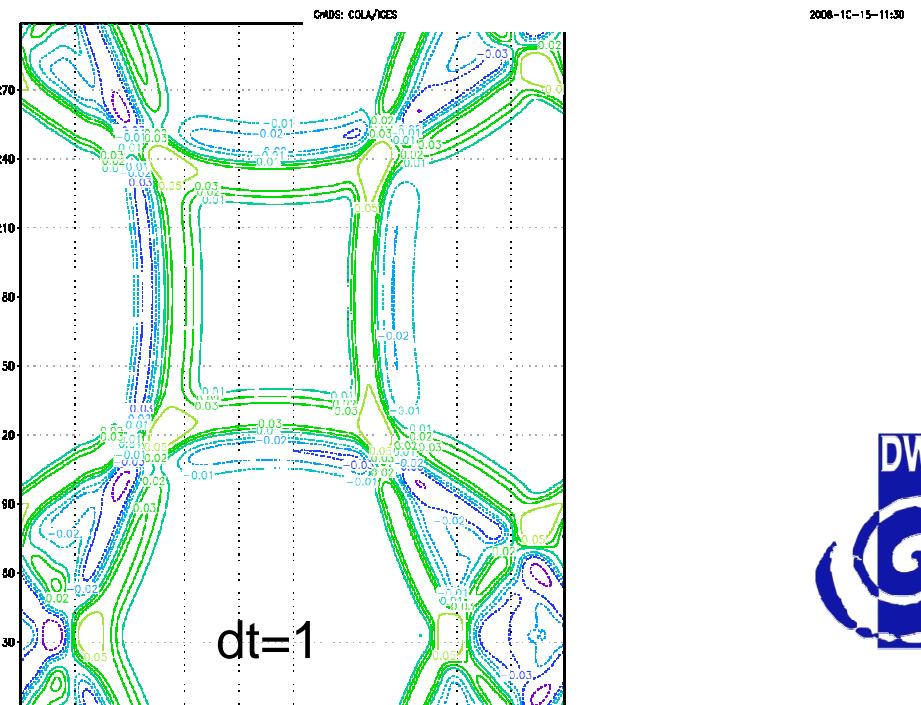
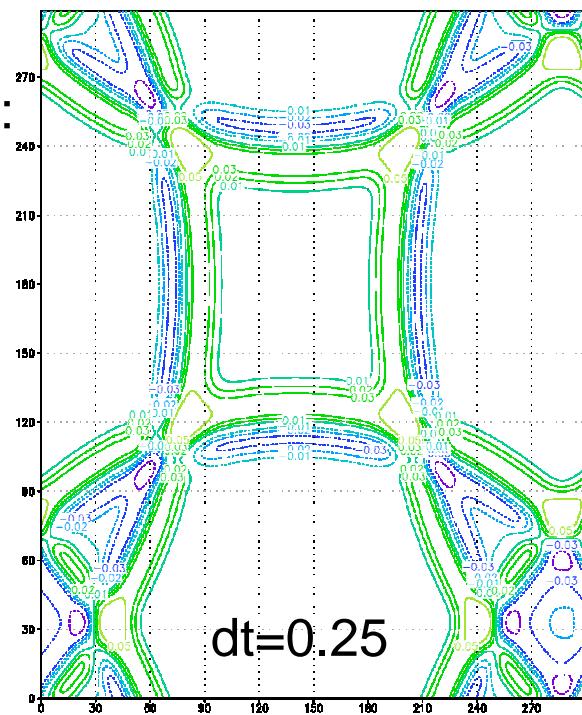
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New scheme:

CN3Crow
in y-direction



GADS: COLA/ICES

2008-10-15-11:38

12



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Do better combinations exist between horizontal and vertical advection?

- complete operator splitting, but with horizontal advection as 'rhs':

$$\frac{\phi^{n+1} - \phi^n}{\Delta t} = \beta A_z(\phi^{n+1}) + (1 - \beta) A_z(\phi^n) + R_x(\phi^n)$$

→ adv. test unstable!

It seems generally not to be a good idea to use explicit parts as a rhs of an implicit scheme

- tendencies of the vertical advection analogous to the physical tendencies
→ adv. test unstable
- implicit scheme only in 3rd RK-sub step → adv. test unstable
- mixing: explicit in RK 1st+2nd sub step, implicit in 3rd RK-sub step
→ adv. test: strongly damping or unstable
- 'partial operator splitting': → adv.tests ok., but shallow water equations unstable

$$\phi^* = \phi^n + \frac{\Delta t}{3} A_x(\phi^n)$$

$$\phi^{**} = \phi^n + \frac{\Delta t}{2} A_x(\phi^*)$$

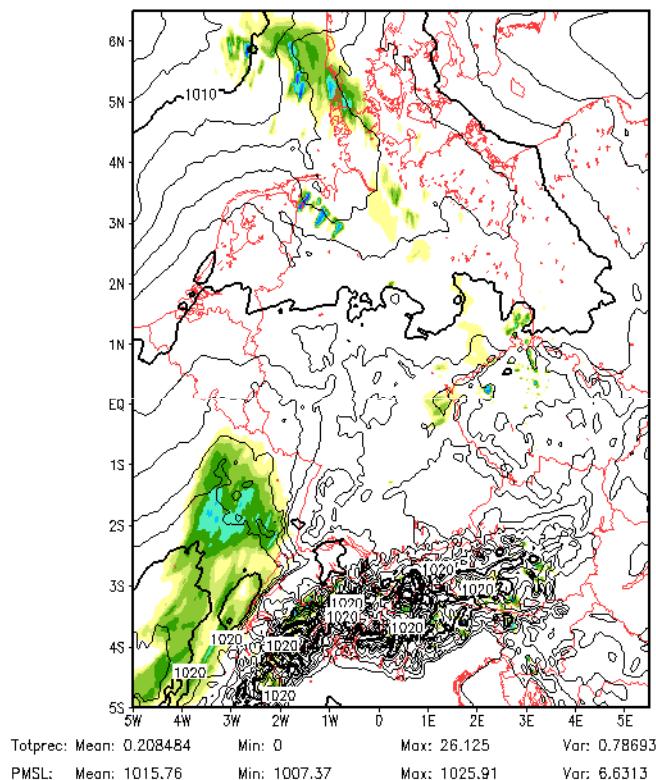
$$\phi^{***} = \phi^n + \Delta t A_x(\phi^{**})$$

$$\phi^{n+1} = \phi^{***} + \Delta t [\beta A_z(\phi^{n+1}) + (1 - \beta) A_z(\phi^{***})]$$

Start time: 01.08.2008 00:00 UTC
Forecast time: 01.08.2008 13:00 UTC
Total precipitation [mm/h] (shaded)

COSMO-DE_Routine_b

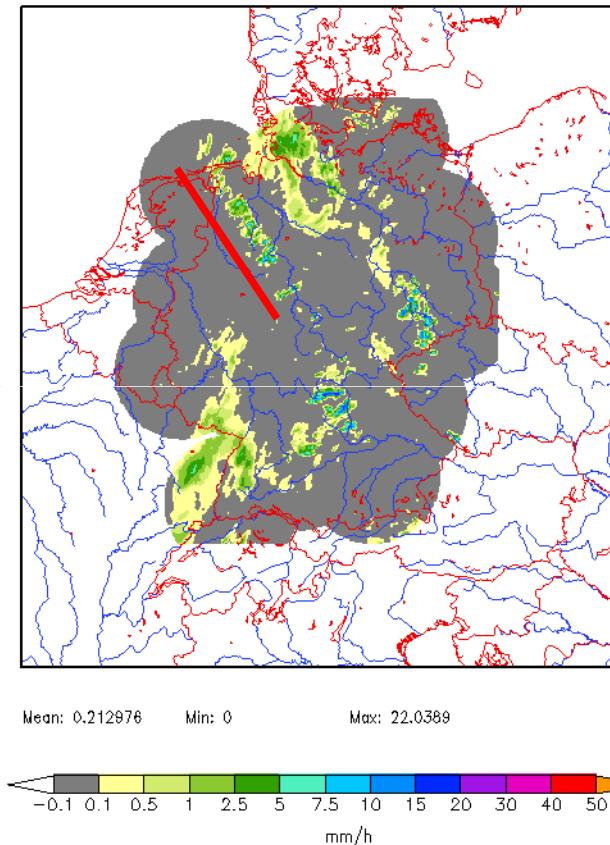
Old VA



RADAR COMPOSITE

valid: 01 AUG 2008 12 – 13 UTC

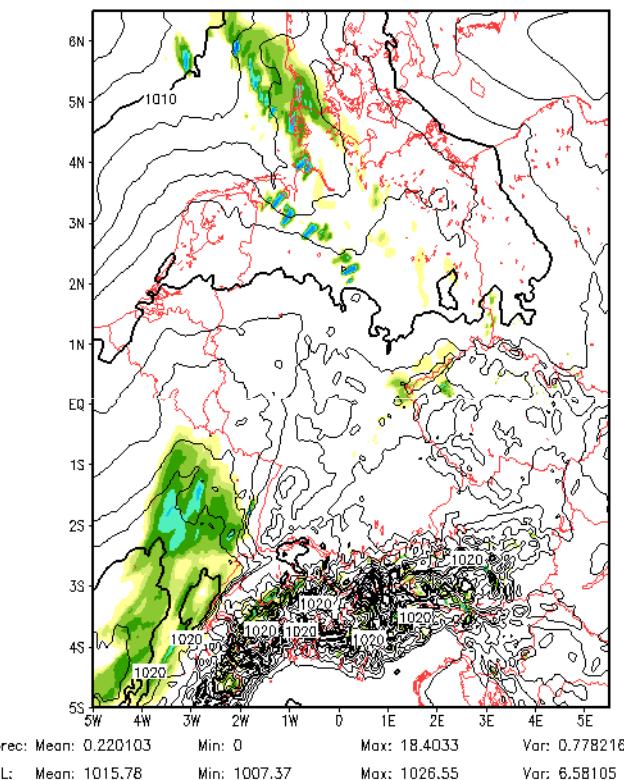
1h PRECIPITATION



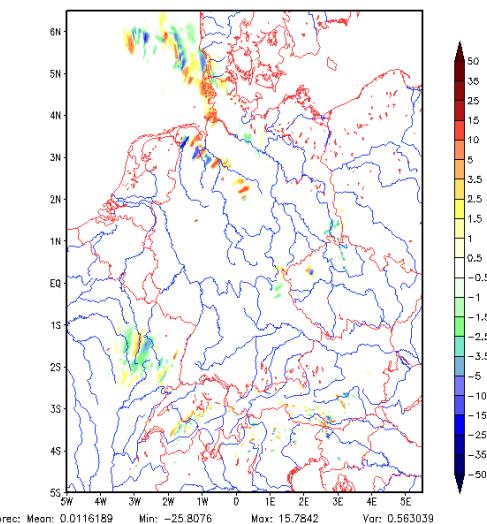
Start time: 01.08.2008 00:00 UTC
Forecast time: 01.08.2008 13:00 UTC
Total precipitation [mm/h] (shaded)

Exp6753Impl_VA

New VA



Diff. ,New - Old VA'



Real case study:
COSMO-DE (2.8 km resolution) for the
,01.08.2008', 0 UTC run
1h-precipitation sum at 13 UTC

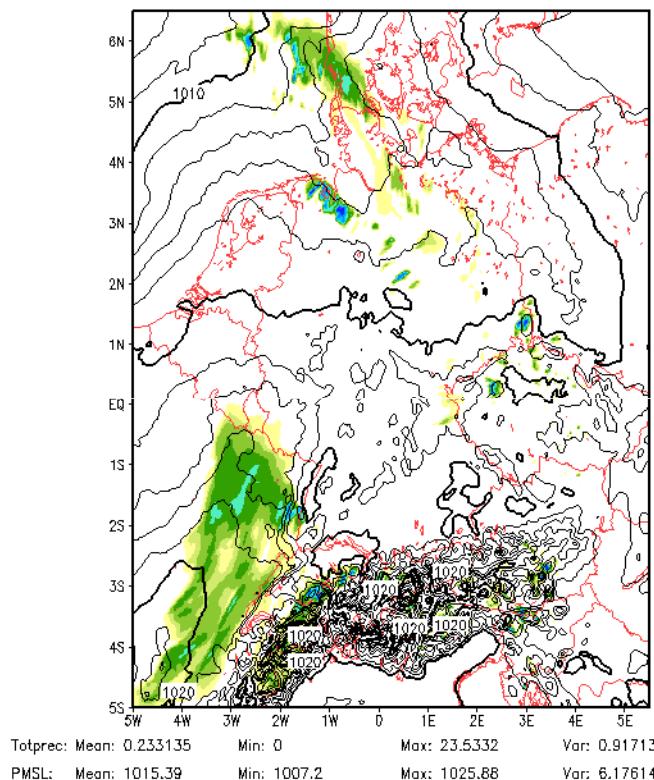
'New VA' = 'Complete operator splitting' with 'CN3Crow'



Start time: 01.08.2008 00:00 UTC
Forecast time: 01.08.2008 14:00 UTC
Total precipitation [mm/1h] (shaded)

COSMO-DE_Routine_b

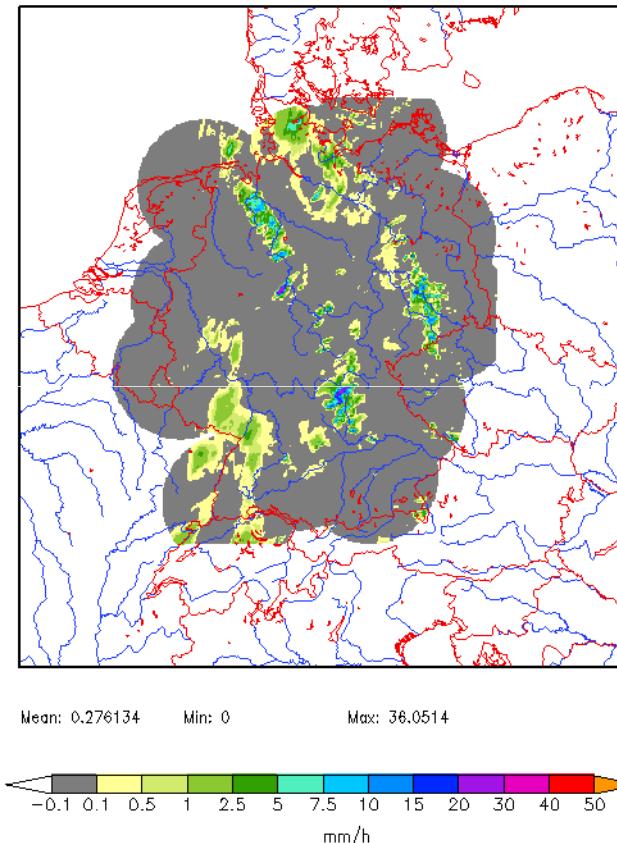
Old VA



RADAR COMPOSITE

valid: 01 AUG 2008 13 – 14 UTC

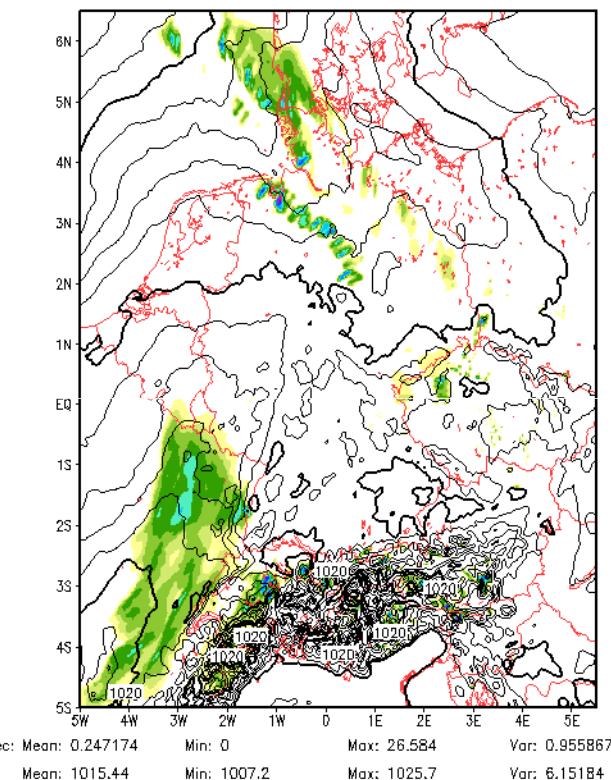
1h PRECIPITATION



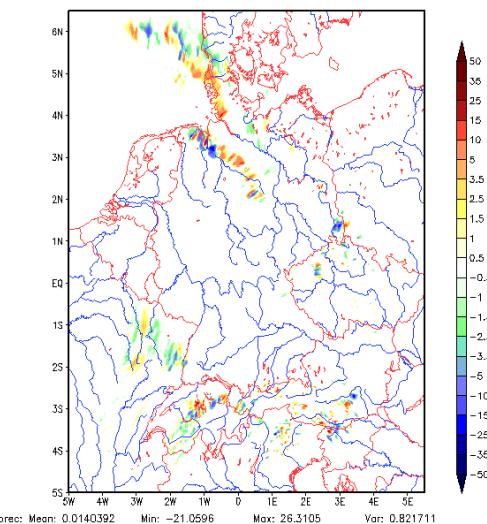
Start time: 01.08.2008 00:00 UTC
Forecast time: 01.08.2008 14:00 UTC
Total precipitation [mm/1h] (shaded)

Exp6753Impl_VA

New VA



Diff. ,New - Old VA'



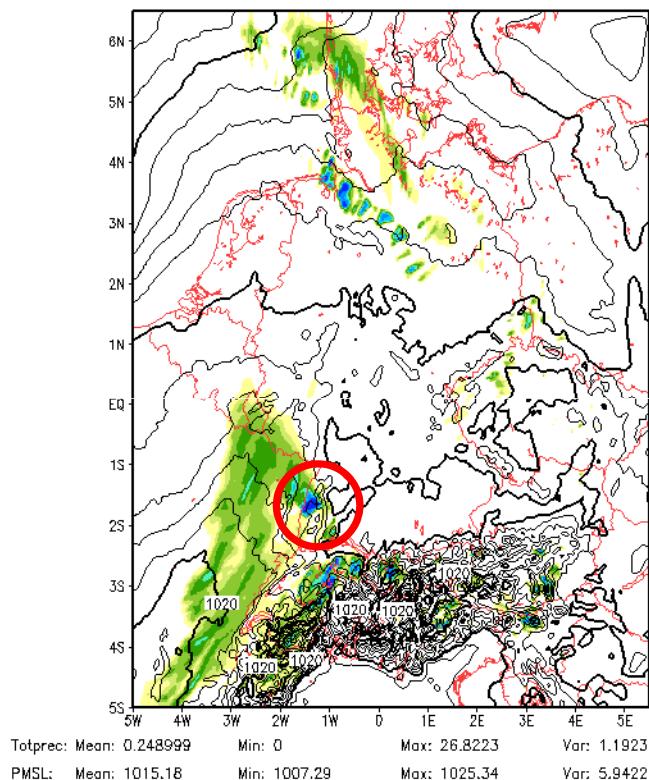
Real case study:
COSMO-DE (2.8 km resolution) for the
,01.08.2008', 0 UTC run
1h-precipitation sum at 14 UTC



Start time: 01.08.2008 00:00 UTC
Forecast time: 01.08.2008 15:00 UTC
Total precipitation [mm/1h] (shaded)

COSMO-DE_Routine_b

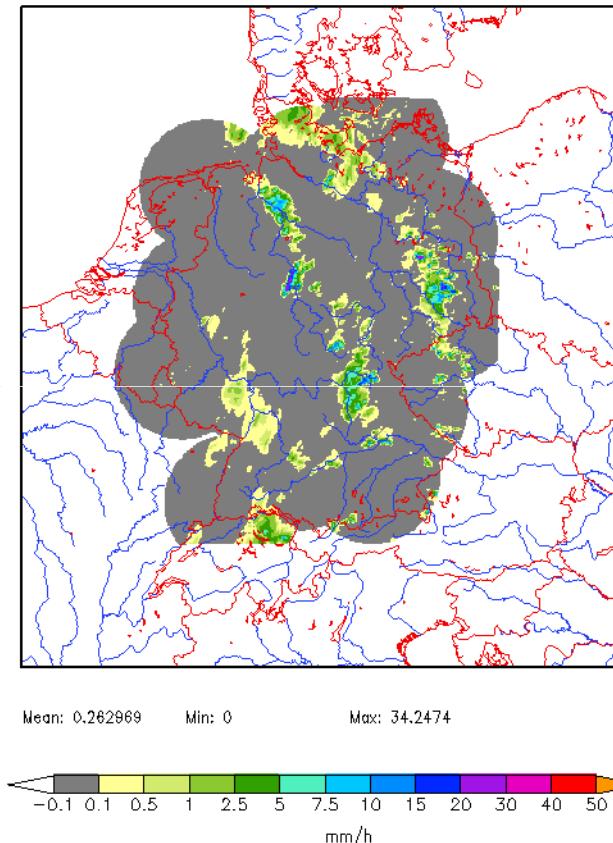
Old VA



RADAR COMPOSITE

valid: 01 AUG 2008 14 – 15 UTC

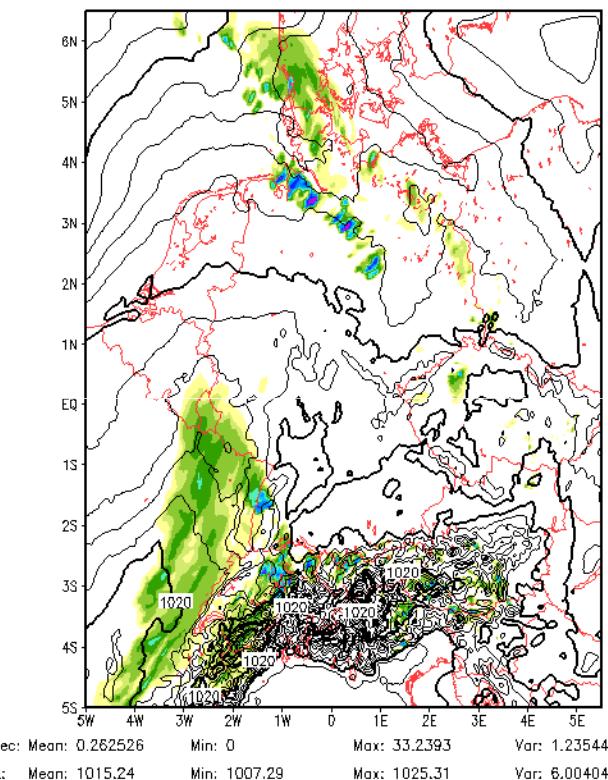
1h PRECIPITATION



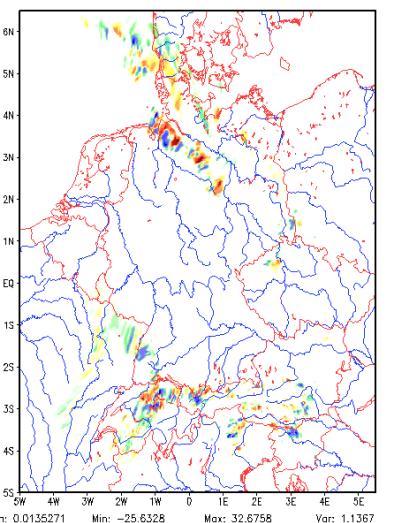
Start time: 01.08.2008 00:00 UTC
Forecast time: 01.08.2008 15:00 UTC
Total precipitation [mm/1h] (shaded)

Exp6753Impl_VA

New VA



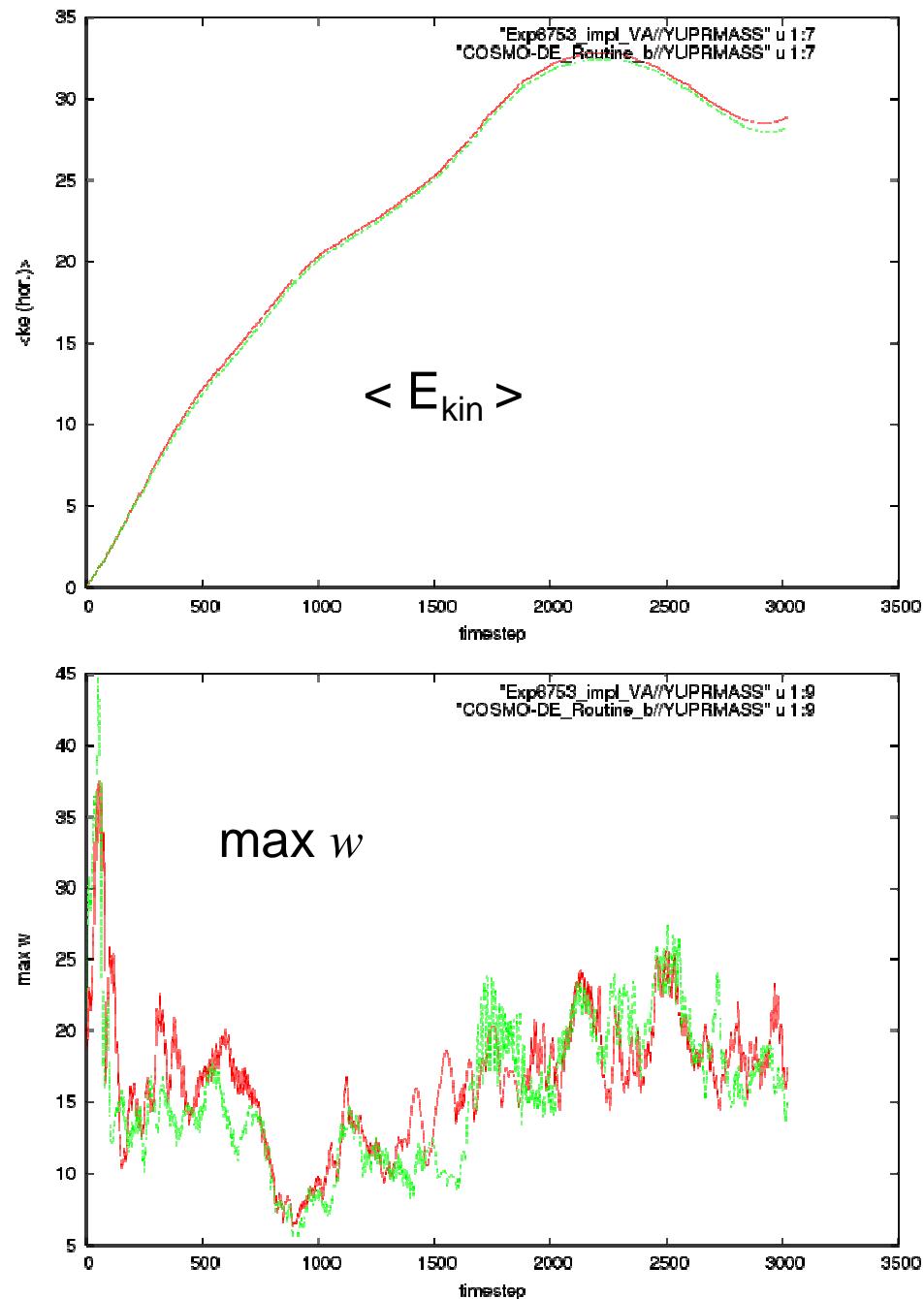
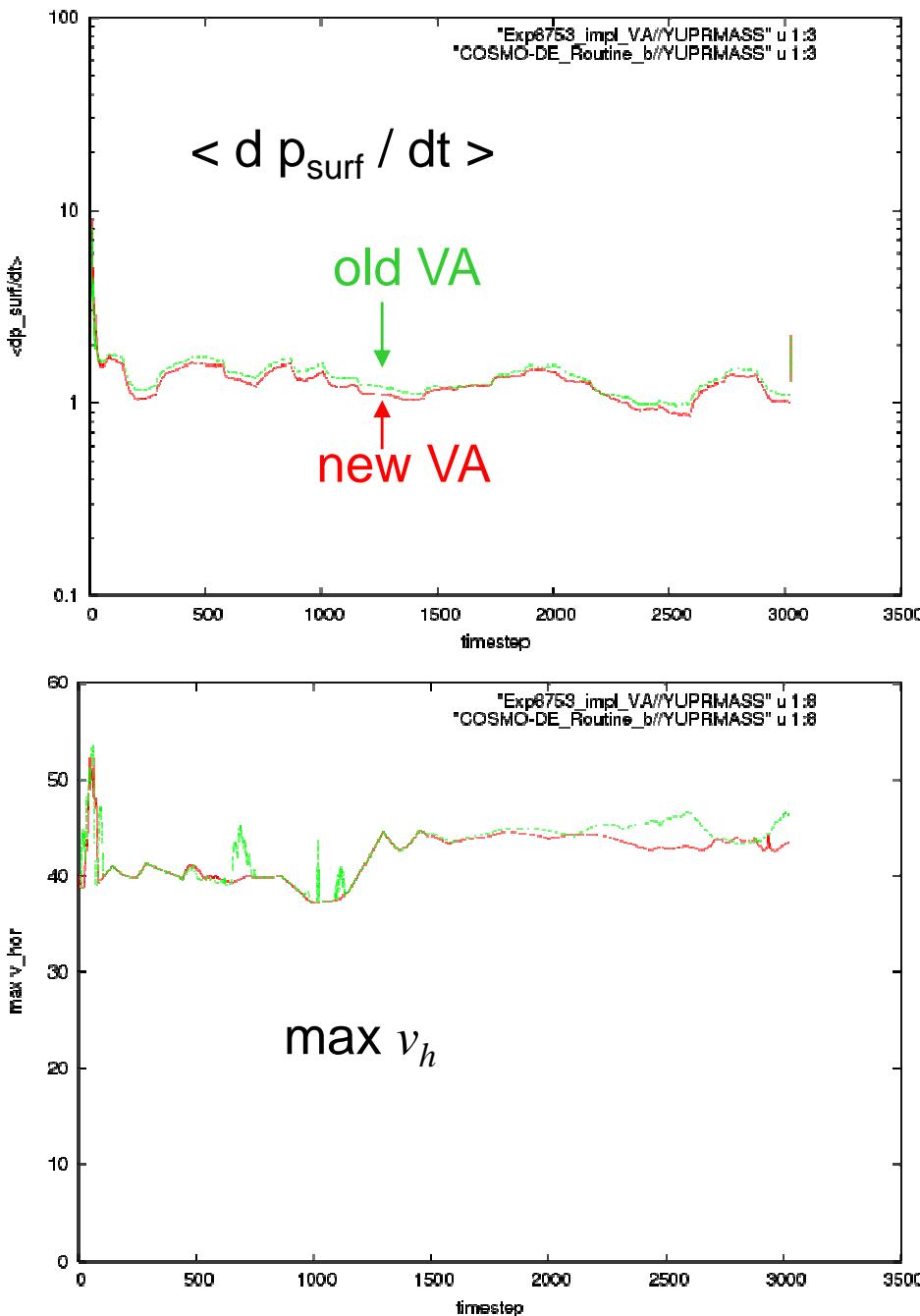
Diff. ,New - Old VA'



Real case study:
COSMO-DE (2.8 km resolution) for the
,01.08.2008', 0 UTC run
1h-precipitation sum at 15 UTC

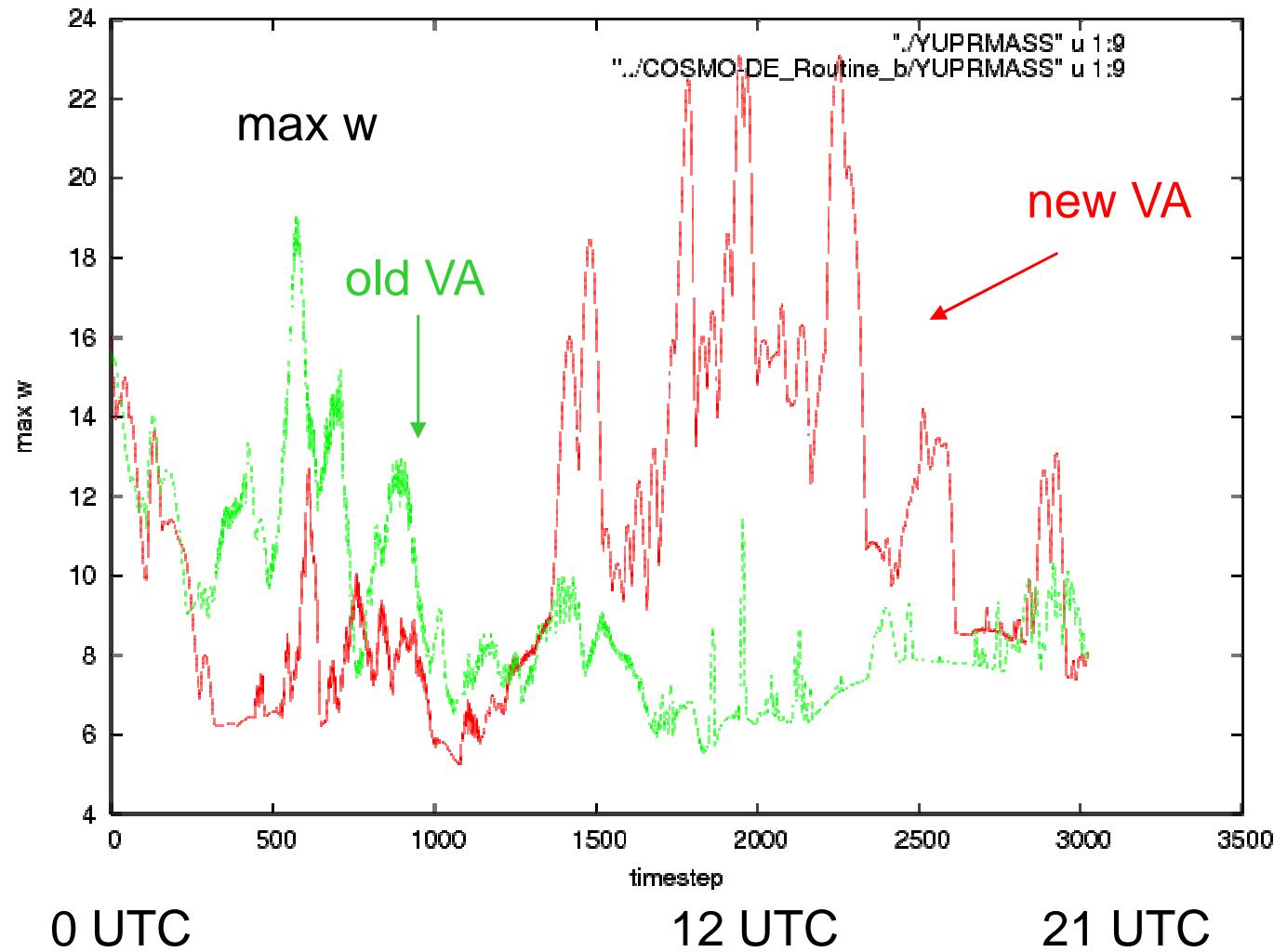


01.08.2008, 0 UTC, mean/max values



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example: 16.08.2008, 0 UTC - run



The new VA sometimes produces higher vertical velocities at noon

0 UTC

12 UTC

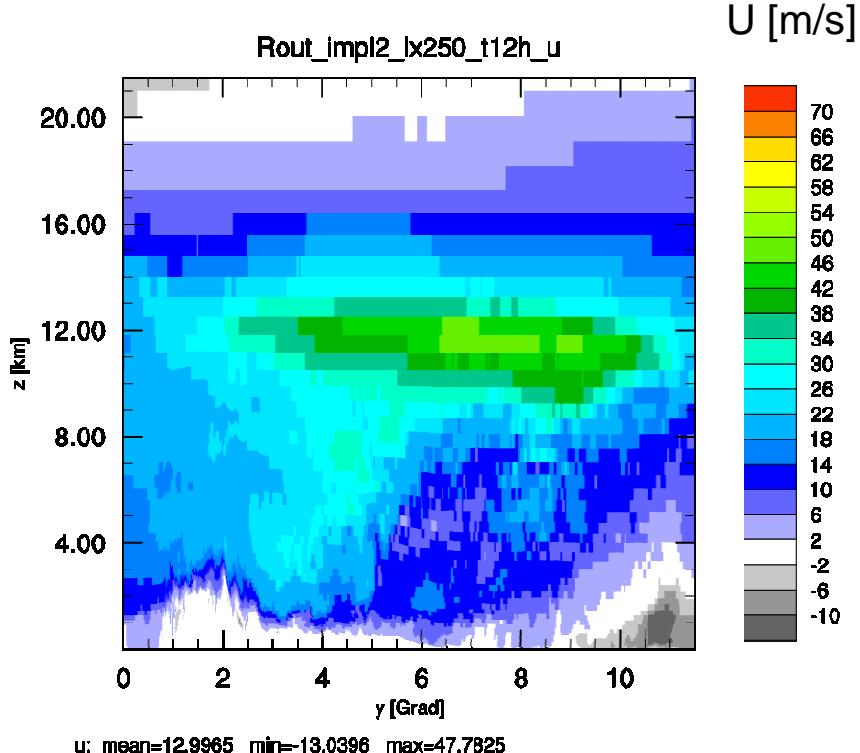
21 UTC

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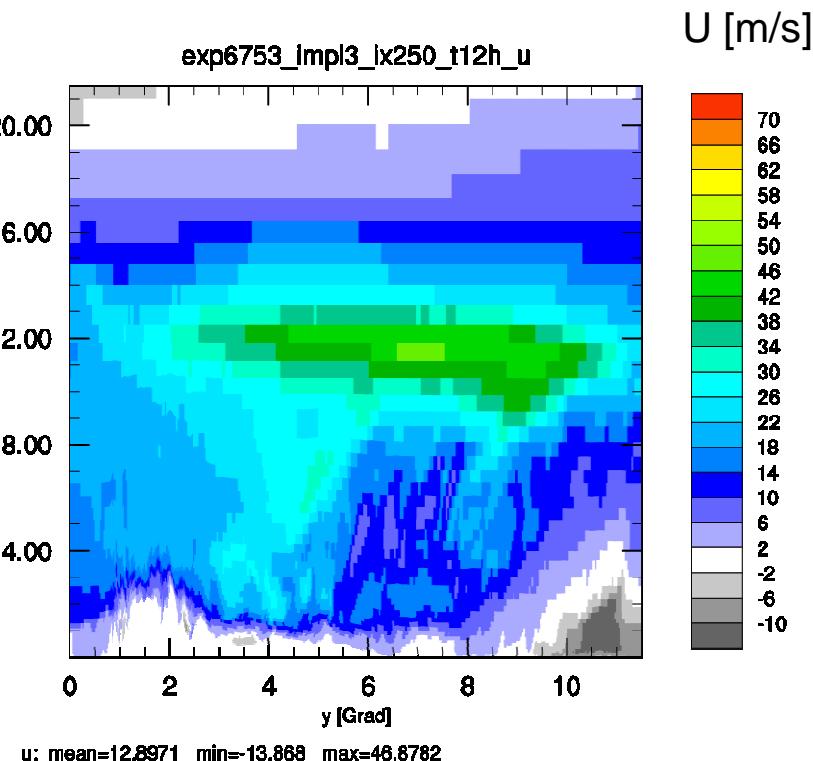
Vertical cross section of zonal velocity

'12.08.2008 0 UTC run' after 12 h

Old VA



New VA



slightly less noisy velocity field

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Summary

The current implicit vertical advection scheme possess a relatively strong damping and is formally not unconditionally stable.

From all of the tested alternatives only the 'complete operator splitting' (= vertical advection outside of the RK-scheme) with CN3 or CN3Crow has proven to be superior:

- improved advection properties in idealized advection tests
- unconditionally stable in C_z
- works also in combination with fast waves
- plausible results in idealized and real cases
- computational amount is only slightly increased
- runs stable for COSMO-DE (2.8 km) simulations during a summer period ('28.07.-21.08.2008')
(an instability at '12.08.' could be cured by an additional calc. of the contravariant vertical velocity)
- stable calculation of a winter time storm event ('10.02.2009')

Outlook

- Synoptic verification
- Correct simulation of inversion layers?



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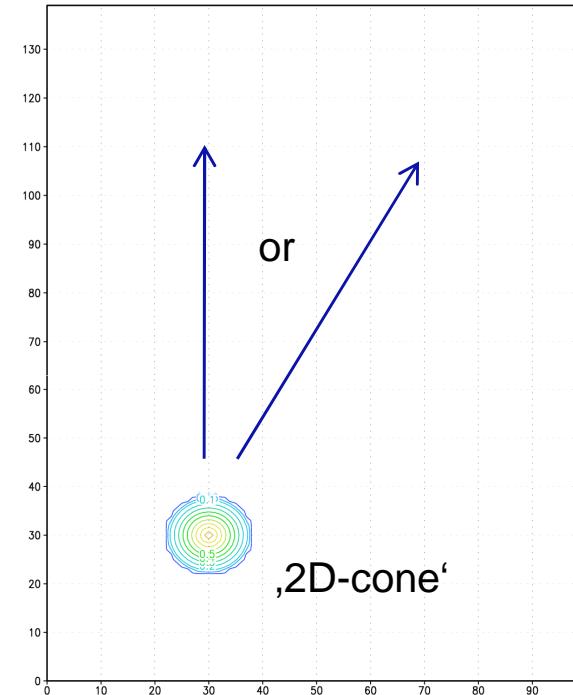
Demonstrate the ability of the implicit schemes: 2D-advection tests

In the following:

- the 3-stage Runge-Kutta is used as time integration scheme
- the horizontal advection always is a 5th order upwind scheme

Wicker, Skamarock, 2002, MWR

Initial state:



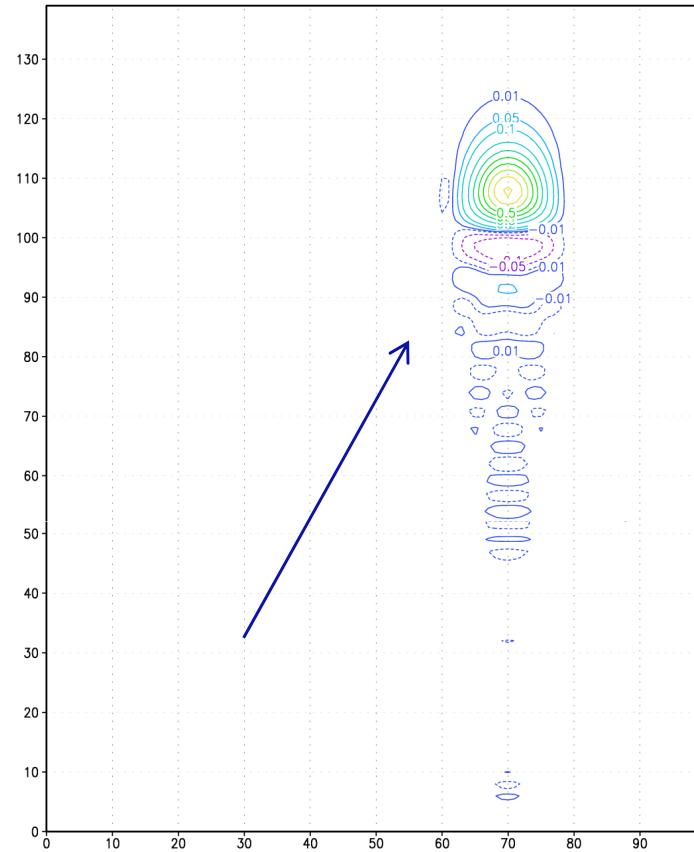
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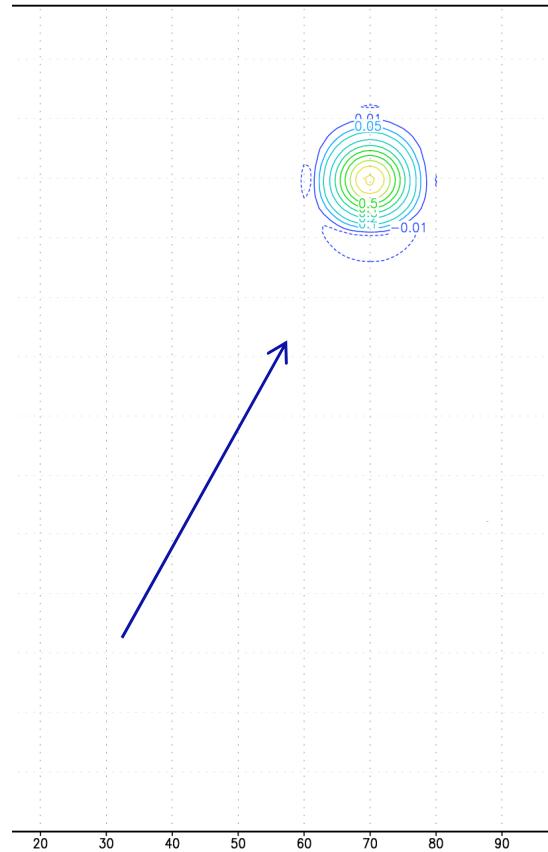
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Complete operator splitting, $dt=0.25 \rightarrow C_z=0.5$

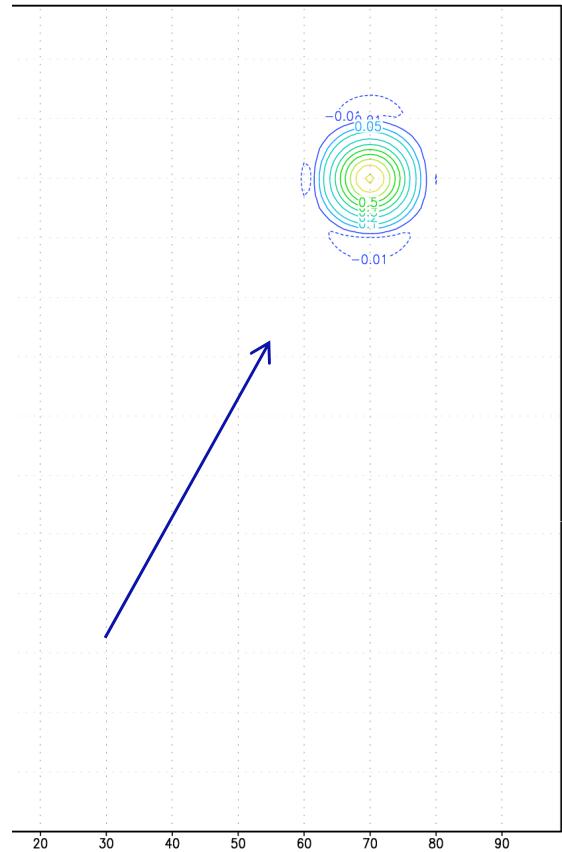
CN2



CN3



CN3Crow



GrADS: COLA/IGES

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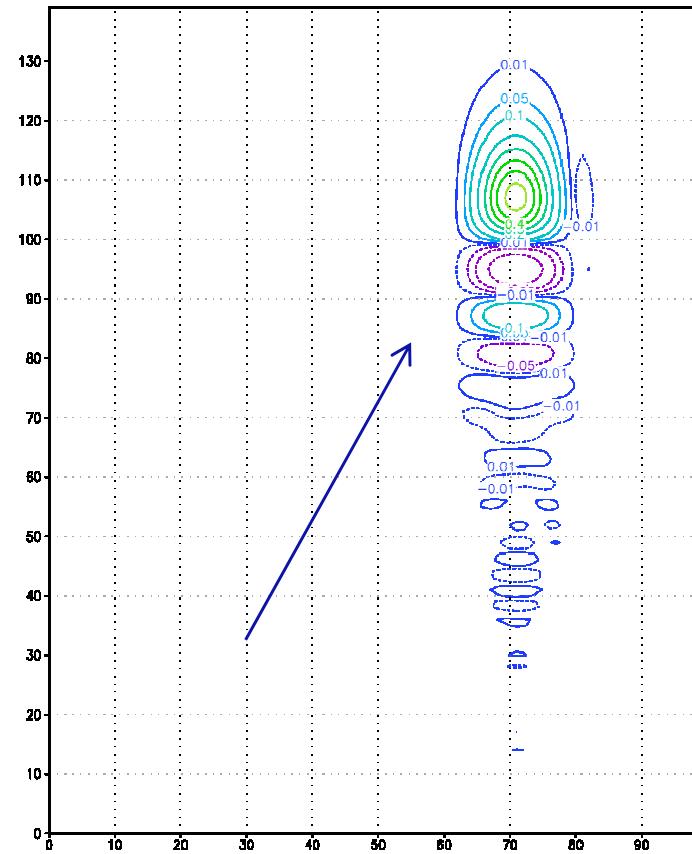
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Test 20081010_a

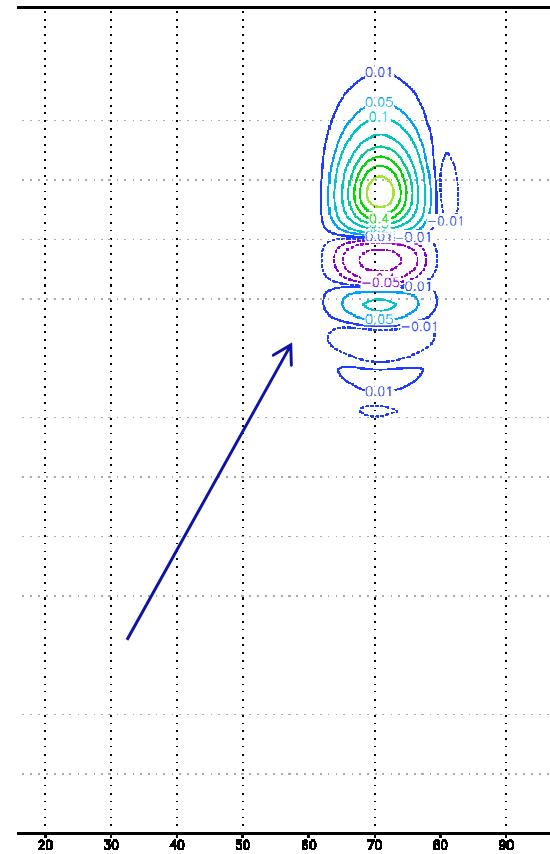
Deutscher Wetterdienst

Complete operator splitting, $dt=1.2 \rightarrow C_z=2.4$

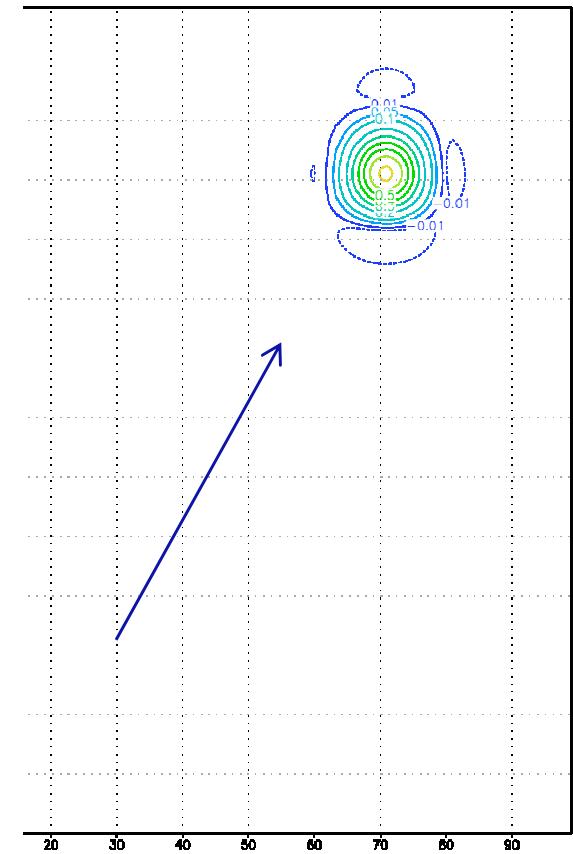
CN2



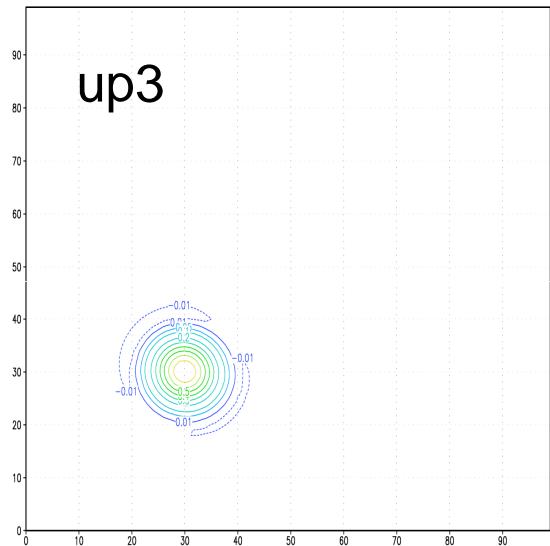
CN3



CN3Crow

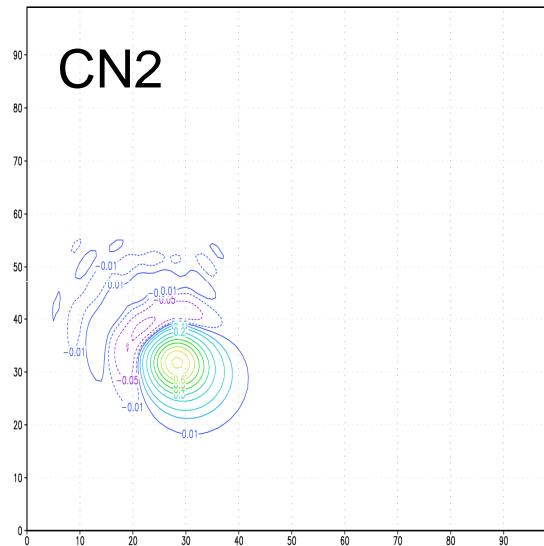


Test 'solid body rotation' (1 turn around)



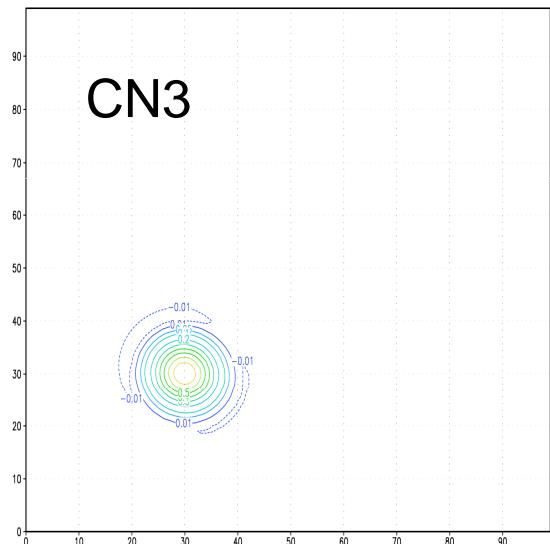
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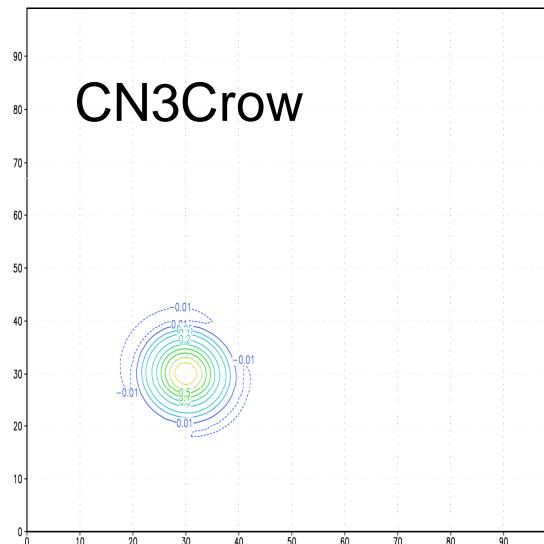
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GADS: COLA/GES

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GADS: COLA/GES

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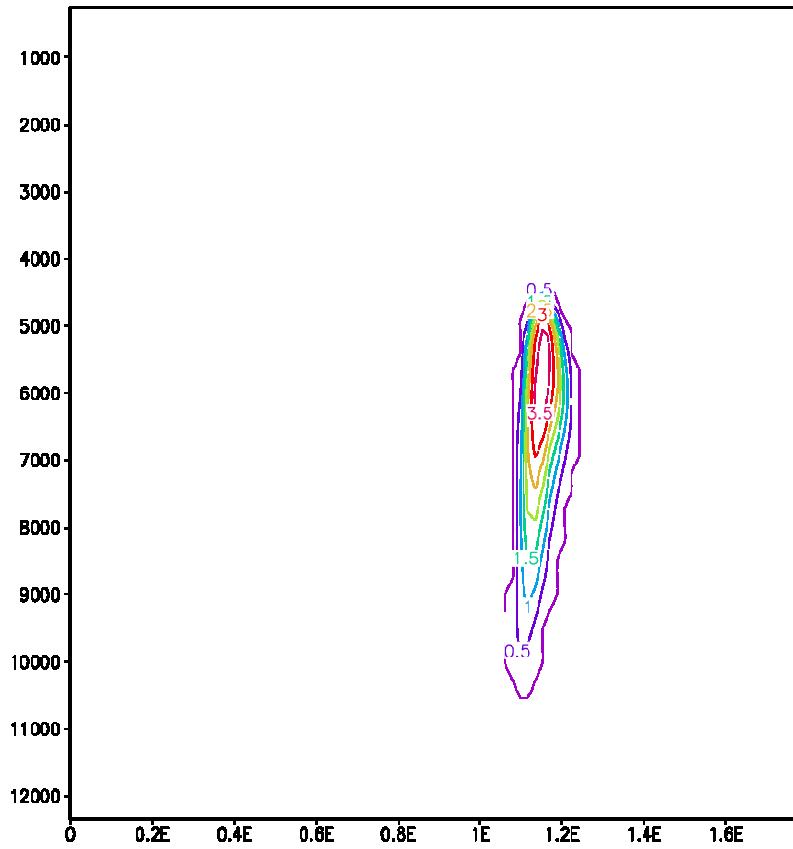
COSMO-model:

behaviour with complete dynamical core (RK3) + simplified physics (only cond./evap.)

Weisman, Klemp (1982)-test case

q_c , after 30 min.

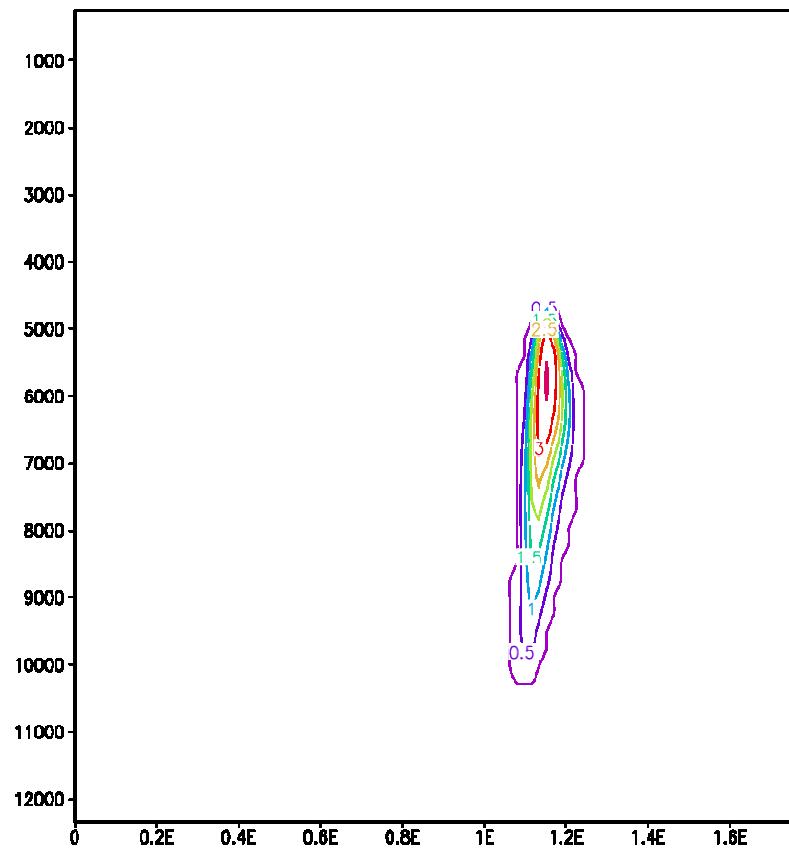
$t=3000[\text{mmss}]$, qc



GrADS: COLA/IGES

CN2 /alt

$t=3000[\text{mmss}]$, qc



GrADS: COLA/IGES

CN3 / kompl. Oper-split.

Efficiency:

CN2 / current scheme:

solves a tridiagonal system: comp. effort ~ 3 N
call in every RK-substep = 3 times / timestep

CN3, ... / complete operator splitting:

solves a pentadiagonal system: comp. effort ~ 13 N
call 1 times / timestep

uses 'Numerical recipes' routines bandec, banbks, which were optimized for vector computers (NEC SX-8R)

gprof: CN2 / bisheriges Schema

ngranularity: Each sample hit covers 4 bytes. Time: 10324.90 seconds

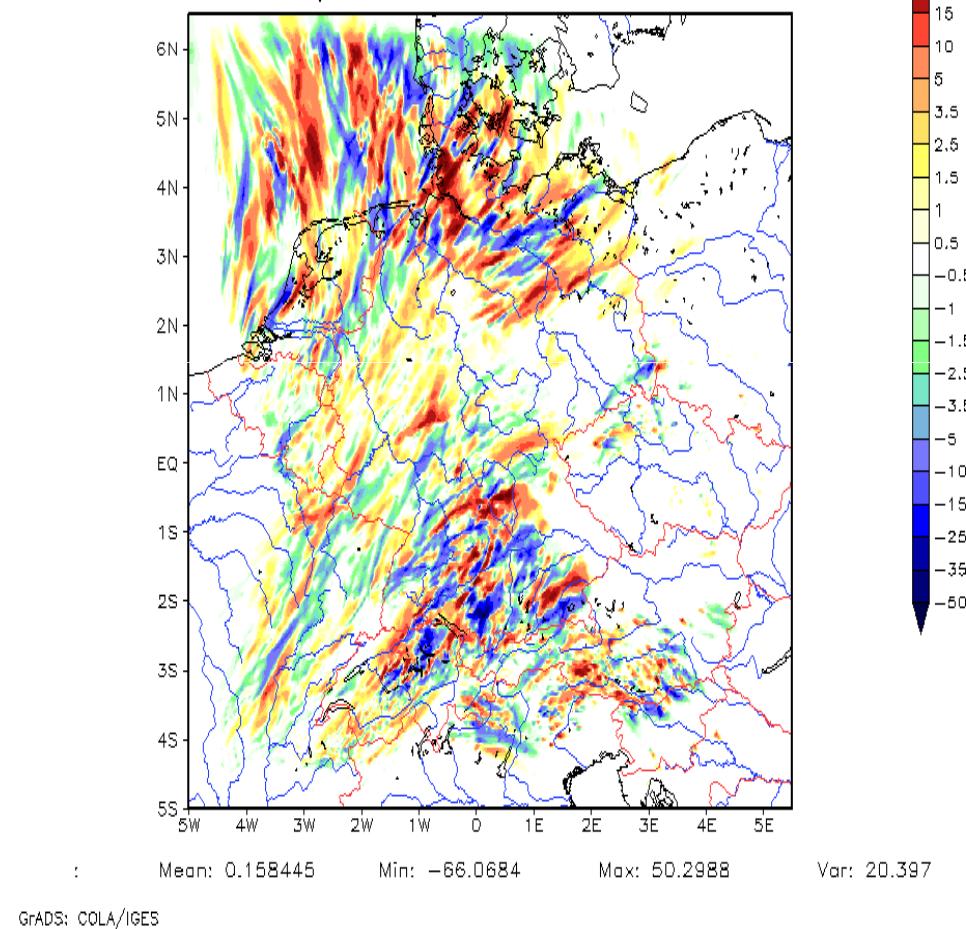
index	%time	self	descendents	called/total		parents	
				called+self		name	index
				called	total		
[4]	57.9	214.25	5765.10	3025	3025/3025	.organize_dynamics [3]	
		214.25	5765.10	3025		.__src_runge_kutta_NM OD _org_runge_kutta [4]	
		2612.57	35.15	9075	9075/9075	fast_waves_runge_kutta [5]	
		17.98	983.63	3025	3025/3025	.__src_advection_rk_NM OD _advection_pd [8]	
		814.85	0.00	9075	9075/9075	complete_tendencies_uvwtpp [10]	
		234.86	305.48	9075	9075/9075	.__src_advection_rk_NM OD _advection [12]	

gprof: CN3Crow / komplettes Operatorsplitting

ngranularity: Each sample hit covers 4 bytes. Time: 10248.44 seconds

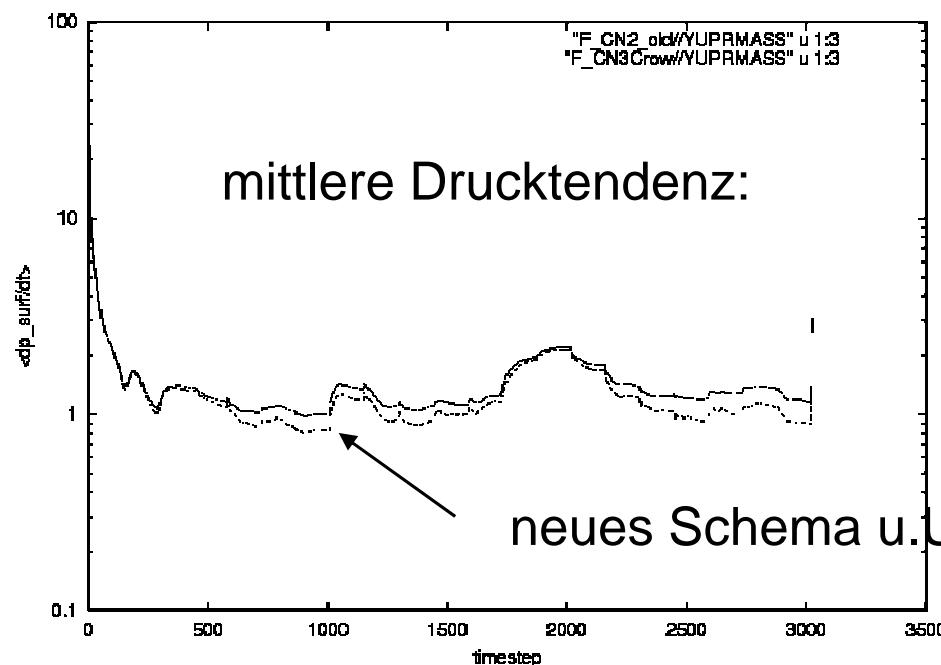
		276.82	5682.12	3025/3025	.organize_dynamics [3]
[4]	58.1	276.82	5682.12	3025	.__src_runge_kutta_NMOD_org_runge_kutta [4]
		2337.45	36.04	9075/9075	.__fast_waves_rk_NMOD_fast_waves_runge_kutta
=====>		248.67	829.96	3025/3025	complete_tend_uvwtp <u>p</u> _cn3crow_nr [7]
		17.02	956.69	3025/3025	.__src_advection_rk_NMOD_advection_pd [9]
		223.75	305.84	9075/9075	.__src_advection_rk_NMOD_advection [13]
		216.53	0.00	3025/3025	implicit_vert_diffusion_uw <u>t</u> [21]
		47.27	141.61	3025/3025	.__hori_diffusion_NMOD_comp_hori_diff [23]
<hr/>					
		248.67	829.96	3025/3025	.__src_runge_kutta_NMOD_org_runge_kutta [4]
[7]	10.5	248.67	829.96	3025	.complete_tend_uvwtp <u>p</u> _cn3crow_nr [7]
		306.41	523.53	15125/15125	.__numeric_utilities_NMOD_solve_5banddiag [11]
<hr/>					
		306.41	523.53	15125/15125	complete_tend_uvwtp <u>p</u> _cn3crow_nr [7]
[11]	8.1	306.41	523.53	15125	.__numeric_utilities_NMOD_solve_5banddiag [11]
		313.96	0.00	59486625/59486625	.__numeric_utilities_NMOD_bandec [18]
		209.46	0.00	59486625/59486625	.__numeric_utilities_NMOD_banbks [22]

diff totprec, 2008080100+21 h



01.08.2008, 0 UTC
21 h precipitation sum
Diff. ,New – Old. VA'





Realer Testfall ('22.08.2008, 0 UTC')

